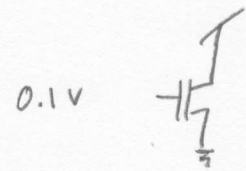
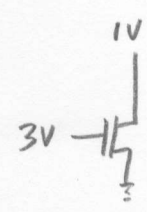


Determine the current flowing in each transistor.

a)  $V_g = 0.1V < V_T \Rightarrow$ Sub V_T operation
 $V_{ds} = V_{dd} - 0V > 100\mu V \Rightarrow$ Saturation

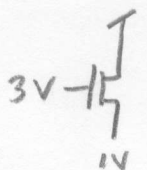
$$I = I_0 e^{\frac{\pi V_g / V_T}{e}} e^{-\frac{V_s / V_T}{e}} e^{\frac{V_d / V_A}{e}} =$$

$$= (1\mu A) e^{(0.65)(0.1V) / (0.0259V)} e^{5V / 50V} = 13.5943 \mu A$$

b)  $V_g - V_s = 3V > V_T \Rightarrow$ Above V_T operation
 $V_d - V_s = 1V$
 $V_{ov} = V_{gs} - V_T = 3V - 0.7V = 2.3V$
 $V_{ds} < V_{ov} \Rightarrow$ Ohmic operation

$$\therefore I = K \left[(V_{gs} - V_T) V_{ds} - \frac{1}{2} V_{ds}^2 \right] =$$

$$= 100 \mu A / V^2 \left[(2.3V)(1V) - \left(\frac{1}{2}\right)(1V)^2 \right] = 180 \mu A$$

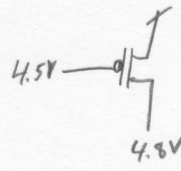
c)  $V_{gs} = 2V > V_T \Rightarrow$ Above V_T operation
 $V_{ds} = 4V > V_{gs} - V_T = 1.3V \Rightarrow$ Saturation
 But what is the actual V_T (we simply used V_{T0} thus far)

Body Effect $\rightarrow V_T = V_{T0} + \gamma \left(\sqrt{V_{sB} + |2\phi_F|} - \sqrt{|2\phi_F|} \right)$
 $V_T = 0.7V + 0.45 V^{1/2} \left(\sqrt{(1V) + |0.9V|} - \sqrt{|0.9V|} \right) = 0.8934V$

Go back and check if our assumptions were correct

$$V_{gs} = 2V > V_T, \quad V_{ds} = 4V > V_{gs} - V_T = 1.1067V$$

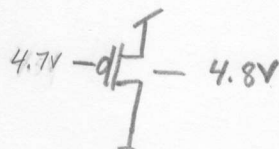
$$I = \frac{K}{2} (V_{gs} - V_T)^2 \left(1 + \frac{V_{ds}}{V_A} \right) = \frac{100 \mu A / V^2}{2} (1.1067V)^2 \left(1 + \frac{5V}{50V} \right) = 67.3632 \mu A$$

d)  $|V_g - V_s| = 0.5V < |V_T| \Rightarrow$ sub V_T operation

$V_s - V_d = 200mV \Rightarrow$ Saturation

$$I = I_0 e^{\alpha(V_w - V_g)/U_T} e^{-\cancel{(V_w - V_s)}/U_T} e^{(V_w - V_d)/V_A}$$

$$I = (1pA) e^{(0.65)(0.5V)/0.0259V} e^{0.2V/50V} = 282.73 nA$$

e)  $|V_g - V_s| = 0.3V < |V_T| \Rightarrow$ sub V_T operation

$V_s - V_d = 5V \Rightarrow$ saturation

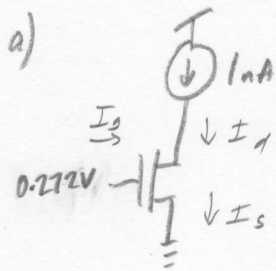
However $V_w = 4.8V$ (back-gate effect)

\rightarrow everything is with respect to V_w

$$I = I_0 e^{\alpha(V_w - V_g)/U_T} e^{-(V_w - V_s)/U_T} e^{(V_w - V_d)/V_A}$$

$$I = (1pA) e^{(0.65)(0.1V)/0.0259V} e^{0.2V/0.0259V} e^{4.8V/50V} = 30.57 nA$$

Determine the DC operating point of each transistor



$$V_g - V_s = 0.275V < V_T \Rightarrow \text{sub } V_T \text{ operation}$$

Start with the assumption of saturated operating (we will verify this)

$$I = I_0 e^{KV_g/UT} e^{V_d/V_A} = 1nA = I_{bias}$$

V_g is known

$$\ln \frac{I_{bias}}{I_0} = \frac{KV_g}{U_T} + \frac{V_d}{V_A}$$

$$V_d = V_A \ln \frac{I_{bias}}{I_0} - \frac{KV_g}{U_T} V_A$$

$$= 50V \ln \left(\frac{1nA}{1pA} \right) - \frac{(0.65)(0.272V)}{0.0259V} (50V)$$

$$= 4.0750V$$

✓ this is in saturation

$$I_g = 0 \quad (\text{no gate current})$$

$$I_D = I_S$$

DC Operating Point

$$V_g = 0.275V$$

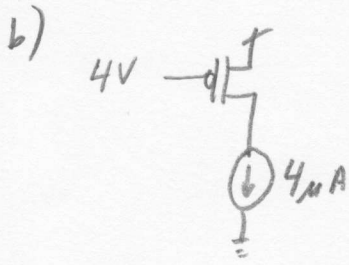
$$I_g = 0$$

$$V_s = 0V$$

$$I_s = 1nA$$

$$V_d = 4.0750V$$

$$I_d = 1nA$$



$$|V_{gs}| = 1V > |V_T|$$

Find the current value at the transition point between ohmic + saturation

(we do not know if this transistor is operating in ohmic or saturation)

$$I = \frac{K}{2} (|V_{gs}| - V_T)^2 = \frac{100 \mu A/V^2}{2} (0.3V)^2 = 4.5 \mu A$$

This current is greater than the current source

∴ The transistor must be operating in the ohmic regime to reduce the current to exactly 4μA.

$$I_{bias} = \frac{K}{2} \left[(|V_{gs}| - V_T)^2 - (|V_{gd}| - V_T)^2 \right]$$

$$|V_{gd}| = \sqrt{\frac{-2I_{bias}}{K} + (|V_{gs}| - V_T)^2} + V_T$$

$$|V_{gd}| = \sqrt{\frac{-(2)4\mu A}{100\mu A/V^2} + (0.3)^2} + 0.7V = 0.8V$$

$$\therefore V_d = V_g + 0.8V = 4.8V$$

DC Operating Point

$$V_g = 4V$$

$$I_g = 0$$

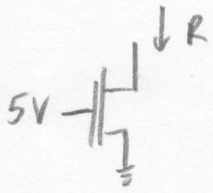
$$V_s = 5V$$

$$I_s = 4\mu A$$

$$V_d = 4.8V$$

$$I_d = 4\mu A$$

a) What value of W causes the MOSFET to have a resistance of 100Ω ?



Given $C_{ox} = 347 \text{ nF/cm}^2$

$L = 1\mu\text{m}$

The transistor is operating in the deep ohmic region

$$I_D = \mu_n C_{ox} \frac{W}{L} (V_{gs} - V_T) V_{ds}$$

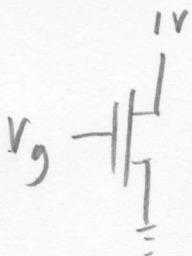
$$R = \frac{V_{ds}}{I_D}$$

$$\therefore R = \frac{1}{\mu_n C_{ox} \frac{W}{L} (V_{gs} - V_T)}$$

$$W = \frac{L}{(R) \mu_n C_{ox} (V_{gs} - V_T)} =$$

$$= \frac{1\mu\text{m}}{(100\Omega) (1460 \text{ cm}^2/\text{Vs}) (347 \text{ nF/cm}^2) (4.3\text{V})} = 4.59 \mu\text{m}$$

b) Determine the bias voltage required to create a $2.5\text{k}\Omega$ resistance, assuming $K = 100 \mu\text{A/V}^2$.



This needs to be operating in above V_T to generate this resistance ($V_{ds} = 1\text{V} \rightarrow$ will not be able to be sub V_T ohmic)

$$V_{gs} > V_{ds} + V_T \quad (\text{or greater to put this transistor into the deep ohmic region})$$

Deep Ohmic (Assumption - we will validate later)

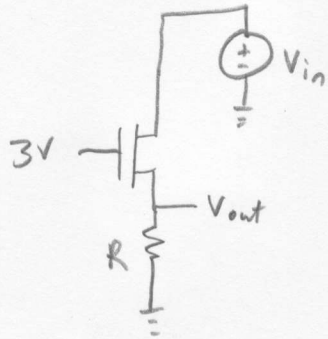
$$R = \frac{1}{K (V_{gs} - V_T)} \Rightarrow V_{ov} = \frac{1}{KR} = \frac{1}{(100 \mu\text{A/V}^2) (2.5\text{k}\Omega)} = 4\text{V}$$

$$\therefore V_{gs} - V_T = 4\text{V} \Rightarrow V_{gs} = 4.7\text{V} \quad \text{This would put the transistor into deep ohmic}$$

Determine V_{out} when sweeping V_{in} from ground to V_{dd}

Assume $\gamma = \lambda = 0$

$I_0 = 0$ (i.e. no sub V_T current)



In ohmic region when

$$V_g - V_{out} - V_T > V_d - V_{out}$$

$$3V - V_{out} - V_T > V_{in} - V_{out}$$

$$3V - V_T > V_{in}$$

$$V_{in} < 2.3V \Rightarrow \text{Ohmic}$$

\therefore For $V_{in} < 2.3V \rightarrow \text{Ohmic}$

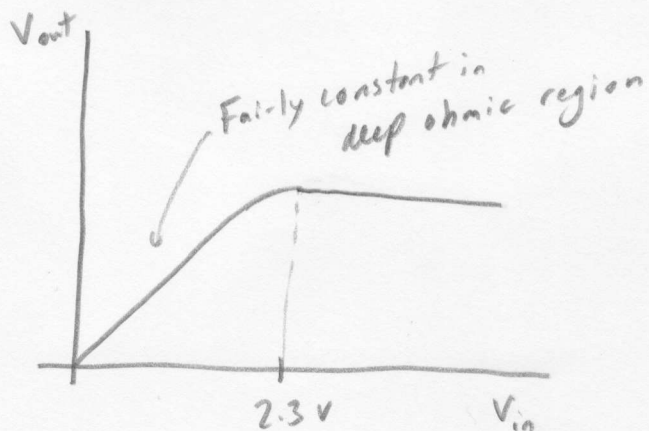
$$V_{out} = I_D R = R K \left[(V_{gs} - V_T) V_{ds} - \frac{1}{2} (V_{gs} - V_T)^2 \right] -$$

$$= R K \left[(2.3V - V_{out})(V_{in} - V_{out}) - \frac{1}{2} (2.3V - V_{out})^2 \right]$$

For $V_{in} > 2.3V \rightarrow \text{Saturation}$

$$V_{out} = I_D R = R \frac{K}{2} (V_{gs} - V_T)^2 = \frac{RK}{2} (2.3V - V_{out})^2$$

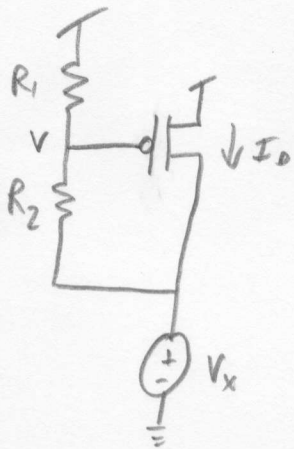
\rightarrow Constant, does not depend on V_{in}



Determine I_D as V_x is swept from ground to V_{dd}

Assume $\gamma = \lambda = 0$

$I_0 = 0$ (no sub V_T current)



$$V = V_{dd} \frac{R_2}{R_1 + R_2} + V_x \frac{R_1}{R_1 + R_2}$$

$$V_{sg} = V_{dd} - V$$

$$= V_{dd} - V_{dd} \frac{R_2}{R_1 + R_2} - V_x \frac{R_1}{R_1 + R_2}$$

$$= \frac{R_1}{R_1 + R_2} (V_{dd} - V_x)$$

$$V_{sd} = V_{dd} - V_x$$

$\therefore V_{sd} \geq V_{sg} \Rightarrow$ If the transistor is turned on, it will be in saturation

Turned on when

$$V_{sg} > |V_T|$$

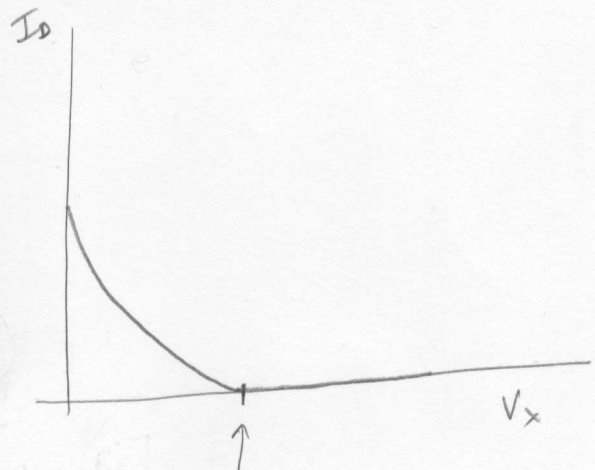
$$\frac{R_1}{R_1 + R_2} (V_{dd} - V_x) > |V_T|$$

$$V_x < V_{dd} - \left(\frac{R_1 + R_2}{R_1} \right) |V_T|$$

Then

$$I_D = \frac{K}{2} (V_{sg} - |V_T|)^2 =$$

$$= \frac{K}{2} \left(\frac{R_1}{R_1 + R_2} (V_{dd} - V_x) - |V_T| \right)^2$$



$$V_{dd} - \frac{R_1 + R_2}{R_1} |V_T|$$