

Harmonic Excitation of Damped Systems Section 2.2

Motorcycle Engine Vibration Problem

A motorcycle engine turns
 (and vibrates) at 300 rpm
 with a harmonic force of 20 N.

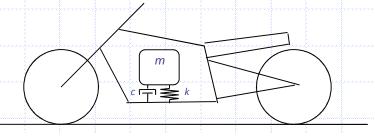
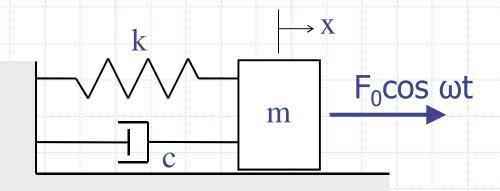


Figure 1. Motor vibrating in motorcycle

- What is the amplitude of the vibration with respect to the frame (assumed to be stationary) and phase of the response (with respect to the force), if:
 - the mass of the engine is 40 kg,
 - the stiffness of the mounts is 40 kN/m and
 - the damping coefficient is 125 Ns/m?

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Damped Spring-Mass System with Forced Vibration



$$m\ddot{x} + c\dot{x} + kx = F_0 \cos \omega t$$

Dividing both sides by *m* yields:

$$\ddot{x} + 2\varsigma\omega_n\dot{x} + \omega_n^2x = f_0\cos\omega t$$

where:
$$f_0 = \frac{F_0}{m}$$

Solving the Differential Equation

Assume a particular solution:

$$x_p(t) = A\cos\omega t + B\sin\omega t$$

so that:
$$\dot{x}_p(t) = -\omega A \sin \omega t + \omega B \cos \omega t$$

$$\ddot{x}_p(t) = -\omega^2 (A\cos\omega t + B\sin\omega t)$$

Substituting into the D.E.:

$$-\omega^2(A\cos\omega t + B\sin\omega t) + 2\varsigma\omega_n\omega(-A\sin\omega t + B\cos\omega t)$$

$$+\omega_n^2(A\cos\omega t + B\sin\omega t) = f_0\cos\omega t$$

Solving the Differential Equation

Separating $\cos \omega t$ and $\sin \omega t$ terms yields:

$$(-\omega^2 A + 2\varsigma\omega_n \omega B + \omega_n^2 A - f_0)\cos\omega t + (-\omega^2 B - 2\varsigma\omega_n \omega A + \omega_n^2 B)\sin\omega t = 0$$

In order to equal zero all the time, both of the constants in front of the $\cos \omega t$ and $\sin \omega t$ terms must equal zero. I.e.:

$$(\omega_n^2 - \omega^2)A + 2\varsigma\omega_n\omega B = f_0$$

$$(-2\varsigma\omega_n\omega)A + (\omega_n^2 - \omega^2)B = 0$$

Solving the Differential Equation

Solving for A and B yields:

$$A = \frac{(\omega_n^2 - \omega^2)f_0}{(\omega_n^2 - \omega^2)^2 + (2\varsigma\omega_n\omega)^2} \qquad B = \frac{2\varsigma\omega_n\omega f_0}{(\omega_n^2 - \omega^2)^2 + (2\varsigma\omega_n\omega)^2}$$

$$B = \frac{2\varsigma\omega_n\omega f_0}{(\omega_n^2 - \omega^2)^2 + (2\varsigma\omega_n\omega)^2}$$

• Substituting for A and B in $x_p(t)$ yields:

$$x_p(t) = \frac{f_0}{\left(\omega_n^2 - \omega^2\right)^2 + \left(2\varsigma\omega_n\omega\right)^2} \left(\left(\omega_n^2 - \omega^2\right)\cos\omega t + 2\varsigma\omega_n\omega\sin\omega t\right)$$

Solving Differential Equation

• Re-writing in terms of X and θ instead of A and B yields:

$$x_{p}(t) = \frac{f_{0}}{\sqrt{(\omega_{n}^{2} - \omega^{2})^{2} + (2\varsigma\omega_{n}\omega)^{2}}} \cos\left(\omega t - \tan^{-1}\left(\frac{2\varsigma\omega_{n}\omega}{\omega_{n}^{2} - \omega^{2}}\right)\right)$$

Final equation (for forced vibration without free vibration):

$$x_{p}(t) = X \cos(\omega t - \theta)$$
where:
$$X = \frac{f_{0}}{\sqrt{(\omega_{n}^{2} - \omega^{2})^{2} + (2\varsigma\omega_{n}\omega)^{2}}}$$

$$\theta = \tan^{-1}\left(\frac{2\varsigma\omega_{n}\omega}{\omega_{n}^{2} - \omega^{2}}\right)$$

Solving Differential Equation

• If we consider both the **free vibration** and **forced vibration** $x(t) = x_h(t) + x_p(t)$, solving for amplitude components in terms of x_0 and v_0 yields:

$$x(t) = e^{-\varsigma \omega_n t} \begin{cases} \left(x_0 - \frac{f_0(\omega_n^2 - \omega^2)}{(\omega_n^2 - \omega^2)^2 + (2\varsigma \omega_n \omega)^2}\right) \cos \omega_d t \\ + \left(\frac{\varsigma \omega_n}{\omega_d} \left(x_0 - \frac{f_0(\omega_n^2 - \omega^2)}{(\omega_n^2 - \omega^2)^2 + (2\varsigma \omega_n \omega)^2}\right) + \frac{2\varsigma \omega_n \omega^2 f_0}{\omega_d \left[(\omega_n^2 - \omega^2)^2 + (2\varsigma \omega_n \omega)^2\right] + \frac{v_0}{\omega_d}}\right) \sin \omega_d t \\ + \frac{f_0}{(\omega_n^2 - \omega^2)^2 + (2\varsigma \omega_n \omega)^2} \left[(\omega_n^2 - \omega^2)\cos \omega t + 2\varsigma \omega_n \omega \sin \omega t\right] \end{cases}$$

Plotting the "Frequency Response"

• Looking at the forced vibration $x_p(t)$, we can plot the amplitude X and phase lag θ as a function of forcing frequency ω .

X

