# **Beam Elements**



Beam with a straight axis (x-axis), with varying cross-section (A(x)), loaded transversely (q(x) in y direction) with transverse deflections (v(x) in y direction).





$$\varepsilon(x) = -\frac{y}{\rho}$$
$$\frac{1}{\rho} \cong \frac{d^2 v}{dx^2}$$

$$\sigma = E\varepsilon = -Ey\frac{d^2v}{dx^2}$$

$$\int_{A} \sigma y dA = \int_{A} -Ey^2 \frac{d^2 v}{dx^2} dA$$

$$\bigvee_{\text{West Virginia University.}} dA$$

$$\int_{A} \sigma y dA = \int_{A} -Ey^{2} \frac{d^{2}v}{dx^{2}} dA \quad \text{Continued from previous slide.}$$

$$M = -EI \frac{d^{2}v}{dx^{2}}$$

$$V = -\frac{dM}{dx} = \frac{d}{dx} EI \frac{d^{2}v}{dx^{2}}$$

$$q(x) = \frac{dV}{dx} = \frac{d^{2}}{dx^{2}} EI \frac{d^{2}v}{dx^{2}} \leftarrow \text{Resulting Field Equation}$$
All 456 Eight Element Applying  $A$ 



Boundary Conditions: Four boundary conditions are necessary to solve a bending problem. Boundary conditions can be:

deflection:	v(0), v(L)
slope:	$\theta(0), \theta(L)$
bending Moment:	M(0), M(L)
shear force:	V(0), V(L)



### **Beam Element – Shape Functions**



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• Recall that shape functions are used to interpolate displacements.

### **Beam Element – Shape Functions**

$$\boldsymbol{v} = \begin{bmatrix} N_1 & N_2 & N_3 & N_4 \end{bmatrix} \begin{cases} \boldsymbol{v}_1 \\ \boldsymbol{\theta}_{z1} \\ \boldsymbol{v}_2 \\ \boldsymbol{\theta}_{z2} \end{cases} = \mathbf{N} \mathbf{d}$$

- There are two degrees of freedom (displacements) at each node: <u>v and  $\theta_{z}$ </u>.
- Each shape function corresponds to one of the displacements being equal to 'one' and all the other displacements equal to 'zero'.
- Note that everything we do in this course assumes that the displacements are small. Institute of Technology

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### **Beam Element – Shape Functions**

$$\sigma = E\varepsilon = -Ey \frac{d^2 v}{dx^2}$$
$$= -Ey \left[ \frac{d^2 \mathbf{N} \mathbf{d}}{dx^2} \right] = -Ey \left[ \frac{d^2 \mathbf{N}}{dx^2} \right] \mathbf{d}$$
$$= -Ey \mathbf{B} \mathbf{d}$$
$$\mathbf{B} = \left[ -\frac{6}{L^2} + \frac{12x}{L^3} - \frac{4}{L} + \frac{6x}{L^2} - \frac{6}{L^2} - \frac{12x}{L^3} - \frac{2}{L} + \frac{6x}{L^2} \right]$$

• Recall that the **B** row vector is used to interpolate stresses & strains.

## **Beam Element – Formal Derivation**

 The formal beam element stiffness matrix derivation is much the same as the bar element stiffness matrix derivation. From the minimization of potential energy, we get the formula:

$$\mathbf{k} = \int_{0}^{L} \mathbf{B}^{T} E I \mathbf{B} \, dx$$

• As with the bar element, the strain energy of the element is given by  $\frac{1}{2}\mathbf{d}^T\mathbf{k}\mathbf{d}$ .



### **Beam Element – Formal Derivation**

The result is:

$$\mathbf{k} = \frac{EI}{L^3} \begin{bmatrix} 12 & 6L & -12 & 6L \\ 6L & 4L^2 & -6L & 2L^2 \\ -12 & -6L & 12 & -6L \\ 6L & 2L^2 & -6L & 4L^2 \end{bmatrix}$$

which operates on  $\mathbf{d} = [v_1, \theta_{z1}, v_2, \theta_{z2}]^T$ .



### **Beam Element – Formal Derivation**

• The moment along the element is given by:

$$M = EI\frac{d^2v}{dx^2} = EI \mathbf{Bd}$$

• The stress is given by:

$$\sigma_x = -\frac{My}{I} = -yE\mathbf{B}\mathbf{d}$$



## **Beam Element w/Axial Stiffness**

• If we combine the bar and beam stiffness matrices, we get a general beam stiffness matrix with axial stiffness.

$$\mathbf{k} = \begin{bmatrix} AE/L & 0 & 0 & -AE/L & 0 & 0 \\ 0 & 12EI/L^3 & 6EI/L^2 & 0 & -12EI/L^3 & 6EI/L^2 \\ 0 & 6EI/L^2 & 4EI/L & 0 & -6EI/L^2 & 2EI/L \\ -AE/L & 0 & 0 & AE/L & 0 & 0 \\ 0 & -12EI/L^3 & -6EI/L^2 & 0 & 12EI/L^3 & -6EI/L^2 \\ 0 & 6EI/L^2 & 2EI/L & 0 & -6EI/L^2 & 4EI/L \end{bmatrix} \begin{bmatrix} u_1 \\ v_1 \\ u_2 \\ u_2 \\ v_2 \\ \theta_{z2} \end{bmatrix}$$



## **Uniformly Distributed Loads**

### Laterally:





## **Equivalent Loadings**





## **Orientating Element in 3-D Space**

 Transformation matrices are used to transform the equations in the element coordinate system to the global coordinate system, as was shown for the bar element.

