# **Beam Elements**



Beam with a straight axis (x-axis), with varying cross-section $(A(x))$ , loaded transversely  $(q(x)$  in y direction) with transverse deflections  $(v(x))$  in y direction).





$$
\mathcal{E}(x) = -\frac{y}{\rho}
$$

$$
\frac{1}{\rho} \equiv \frac{d^2v}{dx^2}
$$

$$
\sigma = E\varepsilon = -Ey\frac{d^2v}{dx^2}
$$

$$
\int_{A} \sigma y dA = \int_{A} - E y^2 \frac{d^2 v}{dx^2} dA
$$
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$$
\int_A \sigma y dA = \int_A - Ey^2 \frac{d^2v}{dx^2} dA
$$
continued from previous slide.  
\n
$$
M = -EI \frac{d^2v}{dx^2}
$$
\n
$$
V = -\frac{dM}{dx} = \frac{d}{dx} EI \frac{d^2v}{dx^2}
$$
\n
$$
q(x) = \frac{dV}{dx} = \frac{d^2}{dx^2} EI \frac{d^2v}{dx^2} \leftarrow \text{Resulting Field Equation}
$$
\n
$$
M = 456 \text{ Evin's Power Analysis}
$$



Boundary Conditions: Four boundary conditions are necessary to solve a bending problem. Boundary conditions can be:





### **Beam Element – Shape Functions**







 $k_{32}$ 

• Recall that shape fur Recall that shape functions are used to interpolate displacements.

### **Beam Element – Shape Functions**

$$
v = [N_1 \ N_2 \ N_3 \ N_4] \begin{Bmatrix} v_1 \\ \theta_{z1} \\ v_2 \\ \theta_{z2} \end{Bmatrix} = \mathbf{N} \mathbf{d}
$$

- There are two degrees of freedom (displacements)at each node: *v* and θ*z*.
- Each shape function corresponds to one of the displacements being equal to 'one' and all the other displacements equal to 'zero'.
- Note that everything we do in this course assumes that the displacements are small. Institute of lechnology

MAE 456 Finite Element Analysis

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### **Beam Element – Shape Functions**

$$
\sigma = E\varepsilon = -Ey \frac{d^2v}{dx^2}
$$
  
=  $-Ey \left[ \frac{d^2 \mathbf{N} \mathbf{d}}{dx^2} \right] = -Ey \left[ \frac{d^2 \mathbf{N}}{dx^2} \right] \mathbf{d}$   
=  $-Ey \mathbf{B} \mathbf{d}$   

$$
\mathbf{B} = \left[ -\frac{6}{L^2} + \frac{12x}{L^3} - \frac{4}{L} + \frac{6x}{L^2} - \frac{6}{L^2} - \frac{12x}{L^3} - \frac{2}{L} + \frac{6x}{L^2} \right]
$$

• Recall that the **B** row vector is used to interpolate stresses & strains.

## **Beam Element – Formal Derivation**

• The formal beam element stiffness matrix derivation is much the same as the bar element stiffness matrix derivation. From the minimization of potential energy, we get the formula:

$$
\mathbf{k} = \int_{0}^{L} \mathbf{B}^{T} E I \, \mathbf{B} \, dx
$$

• As with the bar element, the strain energy of the element is given by  $\frac{1}{2}$ d $^T$ kd.

### **Beam Element – Formal Derivation**

The result is:

$$
\mathbf{k} = \frac{EI}{L^3} \begin{bmatrix} 12 & 6L & -12 & 6L \\ 6L & 4L^2 & -6L & 2L^2 \\ -12 & -6L & 12 & -6L \\ 6L & 2L^2 & -6L & 4L^2 \end{bmatrix}
$$

which operates on  $\mathbf{d} = [\nu_1, \theta_{z1}, \nu_2, \theta_{z2}]^T$ .



### **Beam Element – Formal Derivation**

• The moment along the element is given by:

$$
M = EI \frac{d^2 v}{dx^2} = EI \,\mathbf{B} \mathbf{d}
$$

• The stress is given by:

$$
\sigma_x = -\frac{My}{I} = -yE\mathbf{Bd}
$$



## **Beam Element w/Axial Stiffness**

• If we combine the bar and beam stiffness matrices, we get a general beam stiffness matrix with axial stiffness.

$$
\mathbf{k} = \begin{bmatrix}\nAE/L & 0 & 0 & -AE/L & 0 & 0 \\
0 & 12EI/L^3 & 6EI/L^2 & 0 & -12EI/L^3 & 6EI/L^2 \\
0 & 6EI/L^2 & 4EI/L & 0 & -6EI/L^2 & 2EI/L & \theta_{21} \\
-AE/L & 0 & 0 & AE/L & 0 & 0 \\
0 & -12EI/L^3 & -6EI/L^2 & 0 & 12EI/L^3 & -6EI/L^2 & \theta_{22} \\
0 & 6EI/L^2 & 2EI/L & 0 & -6EI/L^2 & 4EI/L & \theta_{22}\n\end{bmatrix}
$$



## **Uniformly Distributed Loads**

### Laterally:



## **Equivalent Loadings**





## **Orientating Element in 3-D Space**

• Transformation matrices are used to transform the equations in the element coordinate system to the global coordinate system, as was shown for the bar element.

